

AIR CONDITIONING BOOSTER

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ABSTRACT: *The study trying to utilize and allows to harness the natural and free solar energy gotten from the sun by converting the additional free enthalpy gotten as thermal and kinetic energy likewise into useful power; on other words the main concern is increasing the COP. This type of AC will use as much solar energy as is available and convert the solar energy directly to replace the equivalent amount of AC power from the mains provider. Under optimum conditions, this can save up to 25% – 45 % of your mains power usage during the summer. This will be most recent innovation in standalone power saving which is partially free of charge by the Sun. The study aims to renovate the traditional refrigeration system which is normally known as compression refrigeration cycle everywhere in our buildings, so that it can be developed to take advantage of the free solar energy without complicated changes neither a completely demolishing.*

KEYWORD: HVAC, Solar radiation, R 134a, thermodynamics, momentum

INTRODUCTION

Jordan is among of the most enthusiastic developing country to promote utilization of renewable energy, as very well known the solar radiation in Jordan average with in 4500 Wh/ m² to 8000 Wh/m².

More than 300 sunny days in Jordan driving us to think more seriously in renewable energy resources and somehow reduce dependence on oil consumption.

Basic thermodynamics statement that as a greater temperature difference between substances the faster heat flow, so once the refrigerant gas temperature increased then a heat rejection is higher; same what happened when the ambient temperature increases, less heat can be rejected from the air-cooled condenser to the hotter ambient.

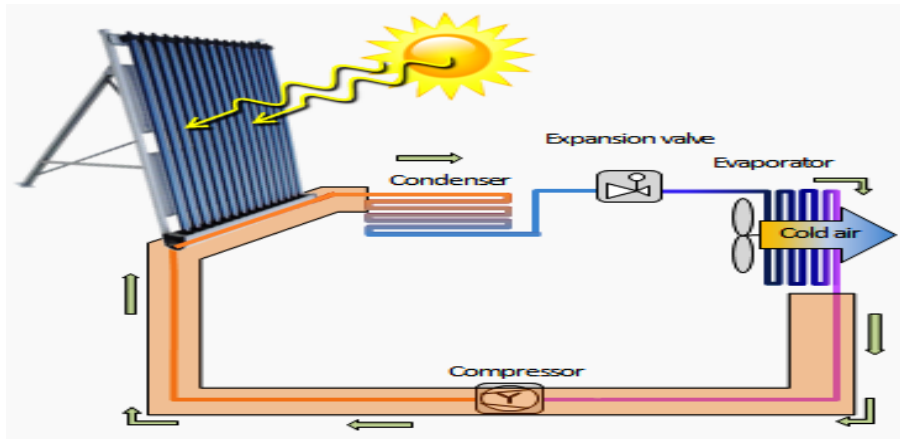


Figure -1

The study here is utilizing thermal energy by using solar collectors see figure - 1.

Adding an extra heat to the cycle in order to increase ΔT between condenser and surrounding environment.

Not quite, but The future will be for renewable energy, however the first step should be renovating the transition phase of the hybridized types by paving the way for the renewable sources, as there is no doubt that renewable energy does not match in any way the traditional energy that we are accustomed to in term of cost neither the required efficiency.

LITRATURE REVIEW

The main point is to drive the point number 2' of the below figure (P-H diagram) to point number 2, in otherwords add a kinetek energy to the system in order to increase the enthlby.

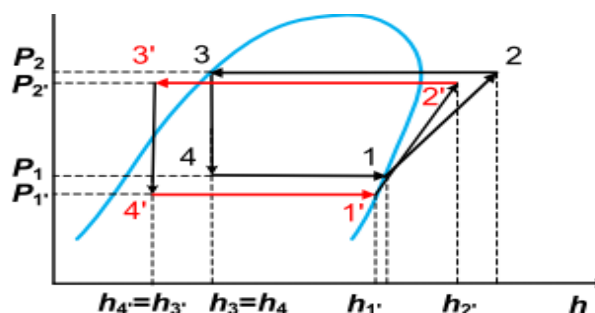


Figure -2

A heat exchanger will be used in this study to reach for a hybrid air conditioning system and achieve to targeted energy savings. By utilizing The First Law of Thermodynamics which is states that heat is a form of energy.

The First Law of Thermodynamics states that energy cannot be created or destroyed; so the sun radiation here or the heat itself will be the exerted energy to the closed refrigeration cycle.

The desired thermal output and rate of heat transfer help determine the optimal type and design of heat exchanger as some heat exchanger designs offer greater heater transfer rates and can handle higher temperatures than other designs.

METHODOLOGY

Heat transferee calculations:

$$\text{a) } Q_h = m_h \times C_{ph} (T_{hout} - T_{hin}) \quad \text{Versus} \quad \text{b) } Q_c = m_c \times C_{pc} (T_{c out} - T_{c in})$$

Equation a here represent water system versus equation b for refrigeration cycle .

Where Q = heat energy (Joules, J) m = mass of a substance (kg) c = specific heat (unit's J/kg·K) Δt is a symbol meaning "the change in" temperatures

T_{cout} = Outlet refrigeration temperature from heat exchanger.

T_{cin} = Inlet refrigeration temperature from heat exchanger.

T_{hin} = Water Inlet temperature from the solar collector to heat exchanger.

T_{hout} = Water outlet temperature from heat exchanger returning to solar collector.

C_{ph} = The specific heat capacity of water is 4.18 kJ/g C.

C_{pc} = Specific isobar heat capacity of R 134 a is 1.7 KJ/Kg.K

m_c & m_h are the mass flow rate of each fluid.

Capacity rate of hot liquid, $Ch = m_h \times C_{ph}$

m_h = mass flow rate of hot water kg/sec; here will be 1 kg/s (Please see note 1)

$$Ch = m_h \times C_{ph} = 1 \times 4.18 = 4.18 \text{ kW/K} \dots\dots\dots (1)$$

$$Cc = m_c \times C_{pc} = 0.2 \times 1.7 = 0.34 \text{ kW/K} \dots\dots\dots (2)$$

It's clear now $C_{min} = C_c = 0.34 \text{ kW/k}$

$$Q_{max} = C_{min} \times (T_{hin} - T_{cin}) = 0.34 \times (85 - 40) = 15 \text{ KW};$$

$$Q_{max} = C_c \times (T_{c\ out} - T_{c\ in}) = 0.34 \times (T_{c\ out} - 40)$$

$$15 \text{ kw} = 0.34 \times (T_{c\ out} - 40) ; \text{ so } T_{c\ out} = 84 \text{ C} \dots\dots$$

$$Q_{max} = C_h \times (T_{h\ in} - T_{h\ out}) = 4.18 \times (85 - T_{h\ out}), \text{ so } T_{h\ out} = 81 \text{ C} \dots\dots$$

$$C_h = m_h \times C_{ph} = 1 \times 4.18 = 4.18 \text{ kW/K} \dots\dots\dots (1) \text{ Please see note 1}$$

$$C_c = m_c \times C_{pc} = 0.2 \times 1.7 = 0.34 \text{ kW/K} \dots\dots\dots (2) \text{ Please see note 2}$$

In order to get mass flow rate of Water (inside heat exchanger) & Refrigerant (R 134 a):

Note 1, For water:

Assuming water inlet 85 c and outlet is 81c :

$$Q = 500 \text{ GPM } \Delta T \text{ (F)}$$

$$15 \text{ KW} / 3.5 = 4 \times 12000 = 51429 \text{ BTU h}$$

51429 / (500 x (185-177)) = 10 GPM Which is 0.7 Kg/s let say = 1 Kg/s to be more reasonable.

Note 2 , For R 134 a :

As discharge temperature almost 40 C so enthalpy is $h_2 = 289 \text{ kJ/kg}$, the same for suction line assume the temperature -10 C so enthalpy is $h_1 = 245 \text{ kJ/kg}$.

Now the refrigerant effect is $h_2 @ T = -40 \text{ C} - h_1 @ T = -10 \text{ C} = h_2 - h_1 = 244.5 - 289 = -44.5 \text{ kJ/kg}$ So for 1 KW we need $1 \text{ (Kj/s)} / 44.5 \text{ (Kj/Kg)} = 0.02 \text{ Kg/s}$; so for 2 refrigeration $T_{on} = 7 \text{ Kw}$ we need :

$$7 \times 0.02 = 0.2 \text{ kg/s}$$

Heat exchanger design:

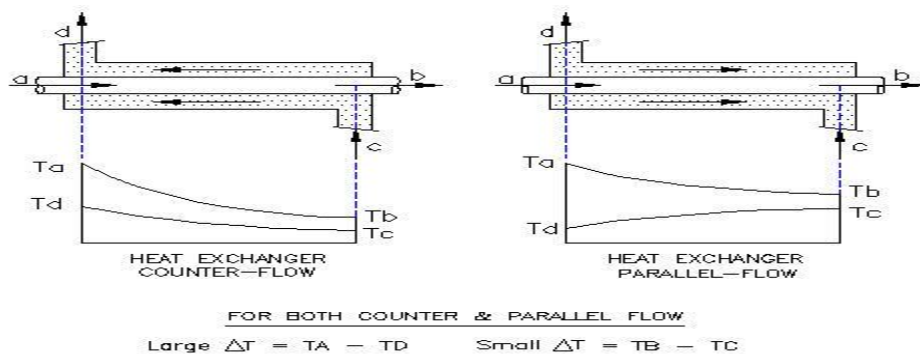


Figure – 3 $U \cdot A \cdot \Delta T_m$

Heat transfer, $Q =$

$$\text{Wall heat transfer coefficient, } U = 1 / (1/h_o + L/K + 1/h_i)$$

Cylindrical wall heat transfer coefficient, $U = 1 / (1/h_i + [Ro \ln(Ro/Ri)]/K + Ri/Ro)$
i and o refer to inside and outside tube surfaces.

$$\begin{aligned} \text{Large temperature difference, } \Delta T_{bc} &= T_a - T_d \\ \Delta T_{bc} &= 19 \quad \text{From Input Data below.} \end{aligned}$$

$$\begin{aligned} \text{Small temperature difference, } \Delta T_{ad} &= T_b - T_c \\ \Delta T_{ad} &= 41 \quad \text{From Input Data below.} \end{aligned}$$

$$\begin{aligned} \text{Logarithmic mean temp. difference, } \Delta T_m &= (\Delta T_{bc} - \Delta T_{ad}) / \ln(T_{bc} / \Delta T_{ad}) \\ \text{Answer: } \Delta T_m &= 28.6 \quad \text{deg C} \end{aligned}$$

The added resistance to heat transfer caused by corrosion is called fouling.
Fouling factor, R ranges between 0.0005 and 0.002. See manufactures data.
Fouling factor, $R = (1/U_{dirty}) - (1/U_{clean})$

Forced Convection - in Coiled Tube Heat Exchangers

Input Data

Turbulent flow in coiled tube.

Temp. of water flowing in, $T_a =$	85	deg C
Temp. of water flowing out, $T_b =$	81	deg C
$T_c =$	40	deg C
$T_d =$	104	deg C
Tube inside diameter, $D_i =$	13	mm
Tube outside diameter, $D_o =$	15	mm
Velocity of water in tube, $V =$	3.5	m / s

Water properties at temperature as per below table:

Water density, $\rho =$	994.7	kg / m ²
$C_p =$	4.183	k*J/kg*K
Water dynamic viscosity, $\mu =$	6.82E-04	kg / m*s
Water conductivity, $k =$	0.6283	W / m*K
Prandtl number, $Pr =$	4.51	-
Factor, $n =$	0.40	
Velocity of water in tube, $V =$	3	m / s

Calculations

$$\begin{aligned} \text{Water bulk temperature, } T_b &= (T_{in} + T_{out}) / 2 \quad \text{deg C} \\ \text{Answer: } T_b &= 83 \quad \text{deg C} \\ \text{Reynolds Number, } Re &= V * D / \nu \\ \text{or, } Re &= V * D * \rho / \mu \end{aligned}$$

Answer: Re =	6.64E+04	Turbulent	Re >4000
Convective heat transfer coefficient, h =	$0.023 \cdot (\text{Re}^{.8}) \cdot (\text{Pr}^n) \cdot (k/d)$		
S.I. Answer: h =	14627	W / m ² *K	
U.S. Answer: h =	$(\text{W}/\text{m}^2 \cdot \text{K})/5.5956$	Btu/hr-ft ² *F	
U.S. Answer: h =	2614	Btu/hr-ft ² *F	
S.I. Answer from above: h =	14627	W / m ² *K	
Large temperature difference, ΔT_{bc} =	$T_b - T_c$		
Answer: ΔT_{bc} =	41	deg C	
Small temperature difference, ΔT_{ad} =	$T_a - T_d$		
Answer: ΔT_{ad} =	19	deg C	
Logarithmic temperature difference, ΔT_m =	$(\Delta T_{bc} - \Delta T_{ad})/\ln(T_{bc}/\Delta T_{ad})$		
Answer: ΔT_m =	28.6	deg C	
Overall heat transfer coefficient =	U_o		
Heat flow rate, Q =	$U_o \cdot A \cdot \Delta T_m$		
Heat flow rate thru inside tube wall, Q_i =	$U_o \cdot \pi \cdot d_i \cdot L \cdot \Delta T_m$		
Heat flow rate thru outside tube wall, Q_o =	$U_o \cdot \pi \cdot d_o \cdot L \cdot \Delta T_m$		
U_o =	$h \cdot A_i / A_o$		
Tube inside area, A_i =	$\pi \cdot d_i \cdot L$		
Tube outside area, A_o =	$\pi \cdot d_o \cdot L$		
Overall heat transfer coefficient, U_o =	$h \cdot d_i / d_o$		
Answer: U_o =	12677	W / m ² *K	
C_p =	$C_p \cdot 1000$		
Answer: C_p =	4183	J/kg*K	
length	Disregarding tube fouling, determine the tube		
The tube length required, L =	$\frac{\rho \cdot V \cdot (d_i)^2 \cdot C_p \cdot (T_{out} - T_{in})}{4 \cdot U_o \cdot d_o \cdot \Delta T_m}$		
Answer: L =	6.21 m		

Efficiency of the system:

$$\eta = \frac{q_{evap}}{w_{comp}} = \frac{h_1 - h_4}{h_{2s} - h_1}$$

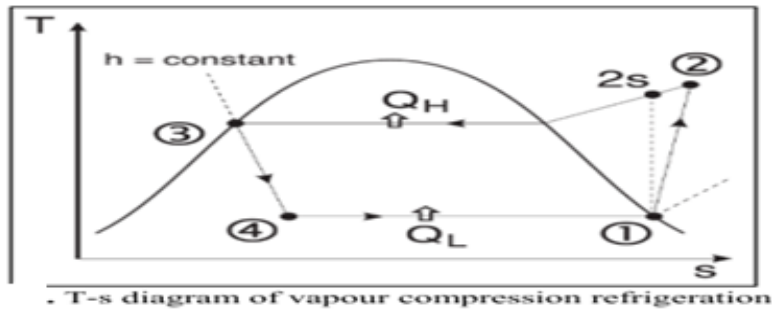


Figure -4

$$W_{comp} = h_{2s} - h_1 = 288 - 242 = 46 \text{ kJ/kg}$$

$Q_{evap} = h_4 - h_1$; as noted @ $T = 90^\circ\text{C}$ & $P = 10 \text{ bar}$, for isenthalpic system $h_3 = h_4 = 38.5 \text{ kJ/kg}$

$$= 38.5 - 242 = -204 \text{ kJ/kg}; \text{ so Efficiency is } = 204/47 = 4.3$$

Now as we used solar energy injected to refrigeration cycle by direct heat exchanging so we have to add the additional gotten enthalpy so,

$$Q_s (2s \text{ to } 2) = h_2 - h_{2s} = 333 - 288 = 45 \text{ kJ/kg}$$

$$\text{So } Q_s + Q_{evap} = 204 + 45 = 249 \text{ kJ/kg}$$

Or

As it's a closed system; The sub cooling add will be the same $h_2 - h_{2s} = h_{3s} - h_3$; by substituting the same parameters then the same values will be gotten.

New COP = $249/46 = 5.5$ which is mean we increase our COP by 25 % from free solar radiation.

However, COP actually is increased more assuming constant pressure during thermal increasing whilst as below I will proof that new pressure has been increased and all values of the above should be taken @ 12 bar instead of 10 bar which is mean COP will be increased up to 35 % more.

SYSTEM DESIGN

The system will be as the below figure:

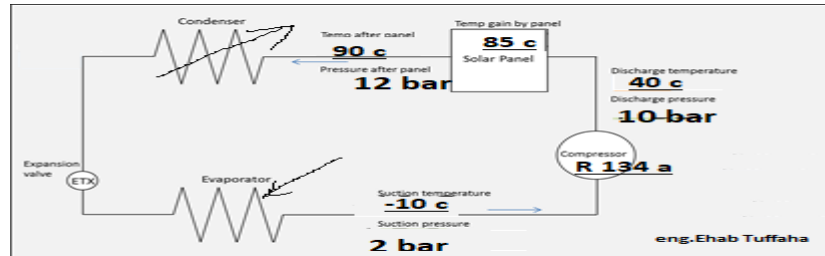


Figure -5

Evacuated heat pipes will be the source of heating, as calculated previously:

Now as previously we got from below equation:

$$Q=500 \text{ GPM } \Delta T \text{ (F)}$$

$$15 \text{ KW} / 3.5 = 4 \times 12000 = 51429 \text{ BTU h } 51429 / (500 \times (185-177)) = 10 \text{ GPM}$$

Which is 0.7 Kg/s let say = 1 Kg/s to be more reasonable.

It seems we need 1 liter in one second so in one minute 60 liters, for factor of safety the tank will be 100 Liter.

Or:

$Pt = (4.2 \times L \times T) \div 3600$. Pt is the power used to heat the water, in kWh, L is the number of litters of water that is being heated and T is the difference in temperature from what you started with, listed in degrees Celsius.

$$\text{We need } 4.18 \text{ kWh} = 15048 \text{ Kj} = m \times 4.18 \times (82-20) = 55 \text{ liter; let say } 100 \text{ liters.}$$

To get evacuated pipe size:

The capacity of each pipe of 58 mm by 1.8 m length almost a 10 liter so we need a 10 heat pipes. Usually each house of 4 persons are requiring from 200 to 300-liter pipe collector so a 100 liter for such process could be connected easily without any new required collectors if we consider the diversity as well to guarantee the water outlet requirements and avoid the **critical temperature of R134a** which is 252 degree Fahrenheit or 122 degrees Celsius.

Mpemba Effect on the Refrigeration Cycle

The basic advantage is a quicker phase change from gas to liquid leading to a better sub cooling and that to less flash gas then more cooling capacity at the evaporator and with the control of the unit then to the original cooling capacity at the evaporator but with less compressor work. All the known formulas in thermodynamics can't explain, because there is really none for the phase change except the amount of heat transferred at phase change.

We gain here 15 KW using our selected heat exchanger); Now a gas coming from a higher temperature has a much higher kinetic energy of the molecules and they kick much more into them as a result they can develop much quicker the interconnecting van der Waals forces and as a result they liquefy quicker. Since the gas gets quicker liquid, the remaining way in the condenser is used to cool down the fully liquid further.

In order to get new pressure @ 90 C =363 k of refrigerant; we have to use Van der Waals force consider the below:

$$\left[P + a \left(\frac{n}{V} \right)^2 \right] \left(\frac{V}{n} - b \right) = RT$$

Where a and b are dimensions to be experimentally found. p = pressure, n= number of moles, T = temperature , V = volume and R = universal gas constant. Hence Its value will be nearby to general gas equation the given gas is at low pressure and high temperature.

$PV = nRT$; $V = A_s \times L$, as the selected exchanger is 0.311 m height ,

$P @ 90 C = 10 \text{ bar} = 9.9 \text{ atm}$; $V = 0.5 \text{ m}^3$

$R = 0.082 \text{ lt. atm / deg.k.mole}$

$10 \times 0.5 = n \times 0.082 \times 363$

So $n = 0.2$

However as very known from

$P_1V = n_1RT \dots$; $P_2V = n_2RT \dots$ Considering the volume is constant (Isochoric) as the heat exchanger is a small closed tank so: $P_2 \times 0.5 = 0.2 \times 0.082 \times 363 \text{ k}$; So $P_2 = 12 \text{ bar}$.

DISCUSSIONS AND IDEAS

Based on the below equations and numbers, a rapidly increasing in momentum during of heating the refrigerant gas R 134a:

As an estimation each pressure drop in heat exchanger 4 m/ 100m and we have a 10 meters pipes so we have a 0.4 bar =4079 kgf/m² (kg per sq. meter); let us multiply the factors as below:

0.2 kg/s (refrigerant flow rate) x 4079 kg/m² x 0.02 m³/kg (specific volume @ 40 c & 2 bar) = 16 kg.m/s

This unit is a momentum, so let us try to get the momentum @ 90 c & 10 bar:

0.2 kg/s (refrigerant flow rate) x 4079 kg/m² x 0.3m³/kg (specific volume @ 90 c & 10 bar) = 245 kg.m/s.

This is mean each change in momentum is a new specific impulse on other words this is producing a thrust force which is also a gain for the cycle.

CONCLUSION

- The system clearly shows that COP is increased from 4.3 to 5.5, by conveting solar thermal energy to subcooling additional for the refrigeration cycle.
- The system adds more 2 bars to the refrigeration cycle consequently increasing in the entropy as mean a quicker phase change due to quicker set-up of intermolecular bindings because of vVan der Waals forces yielding additional sub-cooling.
- The most important is We don't have to increase condenser surface. It is very well capable to remove the additional heat, the Formula $Q = \alpha \times \text{surface} \times \Delta T$. Alpha is heat transfer coefficient and does not change, If Delta T increases due to higher temperature of the refrigerant entering the condenser, the condenser just transfers more heat. The environment as the heat absorbing media is capable of taking up that additional heat. For more explanation, let say what happened with radiators: if you flush water with a temperature of 45°C through the radiator, it does not provide that much heat as if you flush water through with a temperature of 90°C so the radiator is capable of doing the job.

- Basically $W \text{ (KJ/Kg)} = \int p \cdot dv$, however the dv in heat exchanger considered zero by other words it's an Isochoric Work When V is held constant and P changes $W = 0$ Because gas is not doing any work but as surrounding adds energy to internal energy of gas That's why Cp is always greater than Cv Specific heat capacity at constant pressure is always greater than Specific heat capacity at constant volume, now once the gas goes through the condenser a quicker phase change occurred there cause When gas expands it has to do work to push

environment to create space for its expansion by spending energy from its internal energy that's why suddenly Gas cools down.

Suggestions

The below figure shows as condensing temperature increased the efficiency of system will be reduced for all refrigerant gasses except R 717 which is rapidly increased, am suggesting to apply this methodology for such refrigeration cycles with R 717.

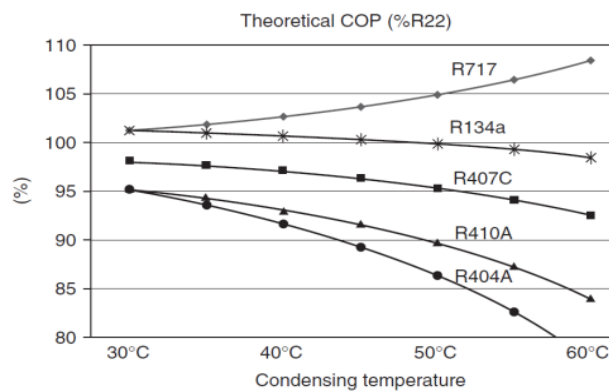


Figure 6

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- Fundamentals of Engineering Heat and Mass transfer by R.C. Sachdeva New age international
- Ron Zevenhoven Åbo Akademi University Thermal and Flow Engineering Laboratory / Värme- och strömningsteknik tel. (02 215)3223 ; ron.zevenhoven@abo.fi.

ADDENDUM

DATA ANALYSIS

The below study shows if reduce refrigerant up to certain limit could be useful for COP, however should we not reach to the maximum temperature of 120 c which is the critical temperature, however power consumption is reduced accordingly.

Water side			R 134 a Side			R 134 a Side			Water side		
Kw/k	kg/s	kJ/kg.k	Kw/k	kg/s	kJ/kg.k	C degree			C degree		
Ch	mh	cph	Cc	mc	cpc	Delat Tc	Tc in	Tc out	Delta Th	Th in	Th out
4.18	1	4.18	0.34	0.2	1.7	45	40	85	3.660287	85	81.33971
4.18	1	4.18	0.238	0.14	1.7	64.28571	40	104.2857	3.660287	85	81.33971

Table 1

The below are a figure out and illustrations using Mollier diagrams which is a very common for systems with fixed compressor speed = fixed mass flow. DC Inverter units with variable mass flows and many changes in circuit offer wide range of mollier diagrams will be a high improvement for the proposed system.

Green = without solar collector:

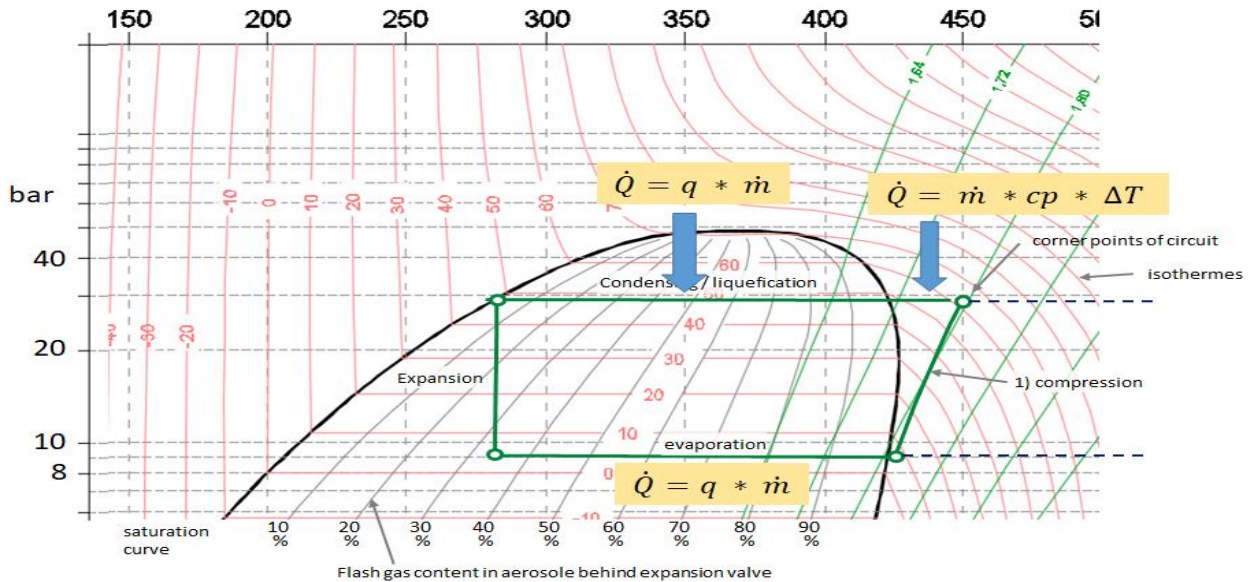


Figure -7

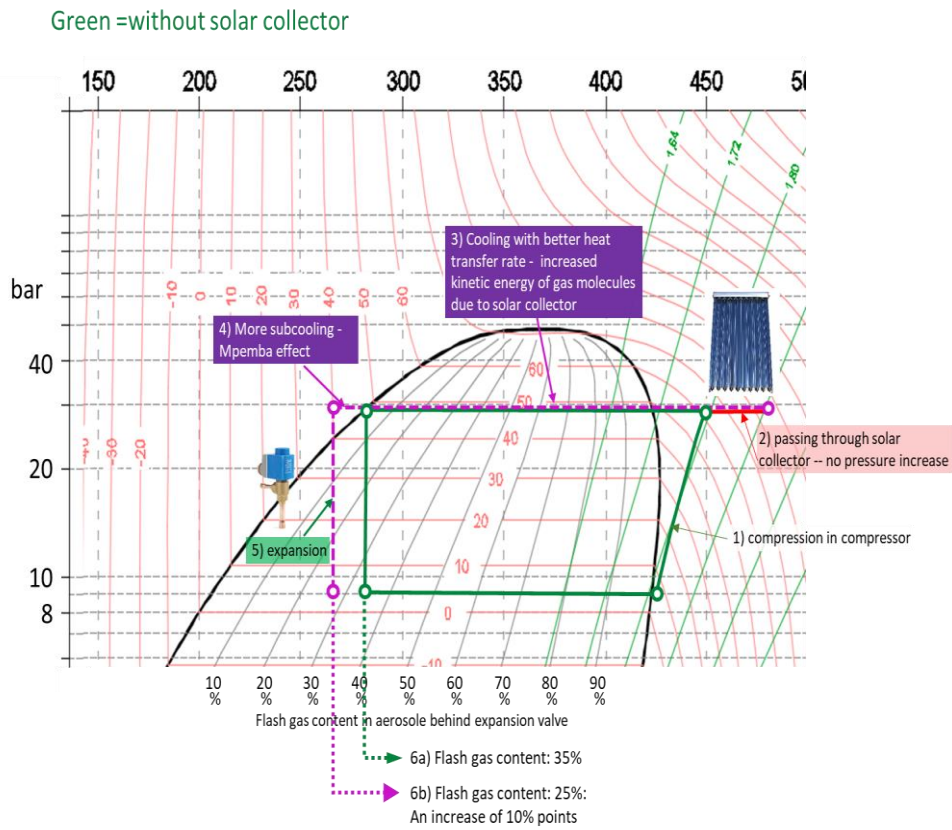


Figure -8

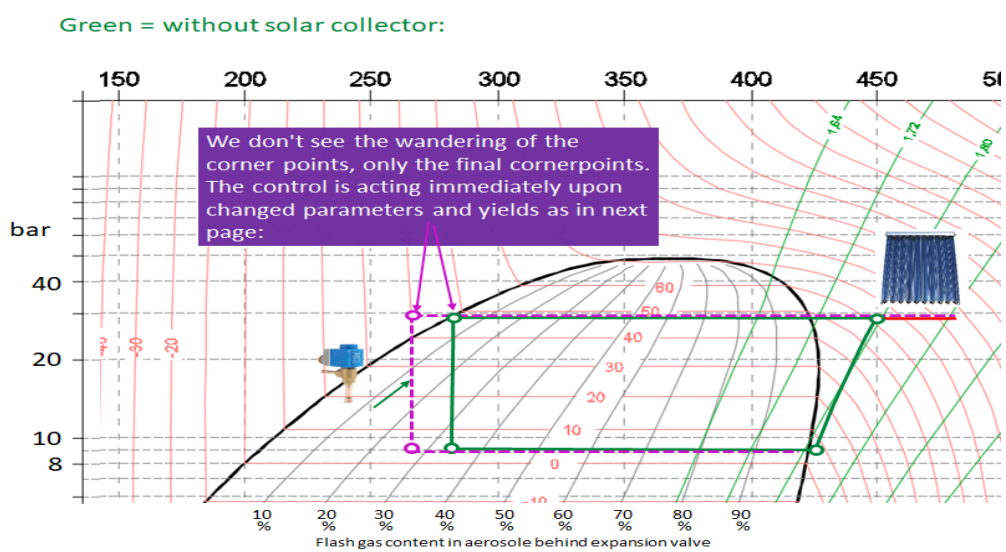


Figure -9

APPENDIX

Figure -1: Illustration of proposed system (By Author).

Figure -2: P-h diagram (Fundamentals and Applications, Fourth Edition by Yunus A. Çengel and Afshin JGhajar).

Figure -3: Heat exchanger design; (Fundamentals and Applications, Fourth Edition by Yunus A. Çengel and Afshin JGhajar).

Figure -4: T-S diagram (Fundamentals and Applications, Fourth Edition by Yunus A. Çengel and Afshin JGhajar).

Figure -5: Illustration of proposed system (By Author).

Figure -6: Refrigerant selection and COP

Figure -7;8 & 9: Mollier diagrams illustrations of proposed system.

Table 1: Spread sheet of applying the same equation in excel sheet. (By author).